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Universiti Tun Hussein Onn Malaysia

**UNIVERSITI TUN HUSSEIN ONN MALAYSIA**

**FINAL EXAMINATION  
SEMESTER II  
SESSION 2017/2018**

**COURSE NAME : ELECTRONIC CIRCUITS  
ANALYSIS AND DESIGN**

**COURSE CODE : BEL 30403**

**PROGRAMME CODE : BEJ**

**EXAMINATION DATE : JUNE/JULY 2018**

**DURATION : 3 HOURS**

**INSTRUCTION : ANSWERS ALL QUESTIONS**

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**THIS QUESTION PAPER CONSISTS OF TEN (10) PAGES**

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**Q1** Analyse the circuit shown in **Figure Q1**,

- (a) Name the function of each Op-Amp, A1, A2, A3, and A4. (2 marks)
- (b) (i) Determine the output for each Op-Amp ( $V_{01}$ ,  $V_{02}$ ,  $V_{03}$  and  $V_{04}$ ). (10 marks)
- (ii) Draw all the waveforms based on answer in part **Q1(b)(i)**. (8 marks)

**Q2** An active filter is shown in **Figure Q2**. Based on this circuit;

- (a) Name the type and order of the filter. (1 mark)
- (b) Formulate the transfer function  $H(s) = V_o(s)/V_i(s)$ . (7 marks)
- (c) Calculate the gain in dB at the passband and determine the cut-off frequencies of this filter when  $R_1 = 3.3 \text{ k}\Omega$ ,  $R_2 = 100 \text{ k}\Omega$ ,  $C_1 = 1.5 \text{ }\mu\text{F}$  and  $C_2 = 68 \text{ pF}$ . (7 marks)
- (d) Sketch the frequency response of the overall filter circuit and label its cutoff frequencies and gain in dB. (5 marks)

- Q3**
- (a) Explain **TWO (2)** differences between system with positive feedback and system with negative feedback. (2 marks)
  - (b) With the aid of a block diagram, derive the closed-loop gain,  $A_f$  of a negative feedback system. (8 marks)
  - (c) An amplifier with a negative feedback has a midband gain of 47.96 dB and low cutoff frequency of 75 Hz. The feedback network of the system has a feedback factor ( $\beta$ ) of 0.0022.
    - (i) Determine the midband gain and the low cutoff frequency if the amplifier does not have a feedback network. (7 marks)

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- (ii) Sketch the frequency response for both systems and label it clearly. (3 marks)

**Q4** (a) (i) Explain the Barkhausen Criterion for an oscillator circuit. (2 marks)

- (ii) Describe the performance of an oscillator circuit if the loop gain falls below 1 and also if the loop gain is greater than 1. (2 marks)

(b) An inverting amplifier circuit using Op-Amp 741 IC, a feedback resistor  $R_F = 145 \text{ k}\Omega$  and input resistance,  $R_A$  is used in a feedback oscillator circuit. The output pin of the amplifier is connected to the three RC network that can generate frequency of oscillation of 50 kHz. Assume that  $R_1 = R_2 = R_3 = R$  and  $C_1 = C_2 = C_3 = C$ .

- (i) Name the oscillator circuit. (1 mark)

- (ii) Draw the oscillator circuit. (3 marks)

- (iii) Using a capacitor value of  $0.001 \text{ }\mu\text{F}$ , design the circuit by finding all other component values. (4 marks)

(c) (i) Design a circuit using 555 timer that will produce an output as shown in **Figure Q4(c)**. Show the complete circuitry with labels. Use a capacitor value of  $0.01 \text{ }\mu\text{F}$ . (6 marks)

- (ii) Calculate the duty cycle. (2 marks)

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- Q5** A voltage regulator circuit with an input voltage ( $V_i$ ) of 36 V and regulated output voltage ( $V_o$ ) of 24 V is shown in **Figure Q5**.

The Zener diode used is 1N4733A which has the following parameters:

$$V_Z = 5.1 \text{ V} \quad I_{Z(\min)} = 1 \text{ mA} \quad I_{Z(\max)} = 178 \text{ mA}$$

The transistor's parameters:  $I_{C(\min)} = 1 \text{ mA}$  and  $I_{C(\max)} = 80 \text{ mA}$ .

- (a) Design the voltage regulator circuit shown in **Figure Q5**. Find the values of  $R_A$ ,  $R_B$ , and range of  $R_S$  that can be used in the circuit, such that the regulated output voltage is maintained at 24 V. (9 marks)
- (b) Determine the power rating for the transistor to be used in the circuit. Assume the input voltage ( $V_i$ ) is fixed at 36 V. (6 marks)
- (c) Explain the operation of the circuit as a voltage regulator when the regulated output is slightly increased from the stated regulated value. (5 marks)

- END OF QUESTIONS -

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SEMESTER / SESSION : SEM II / 2017/2018  
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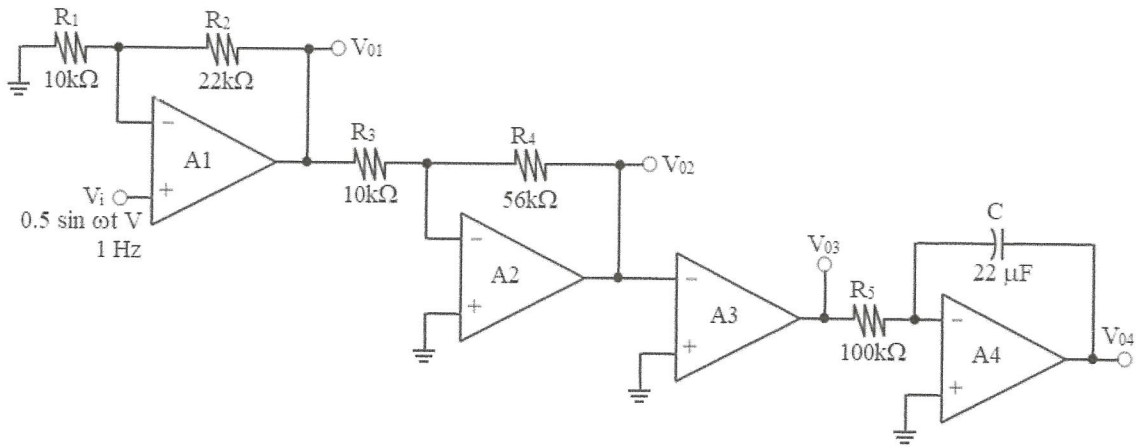


Figure Q1

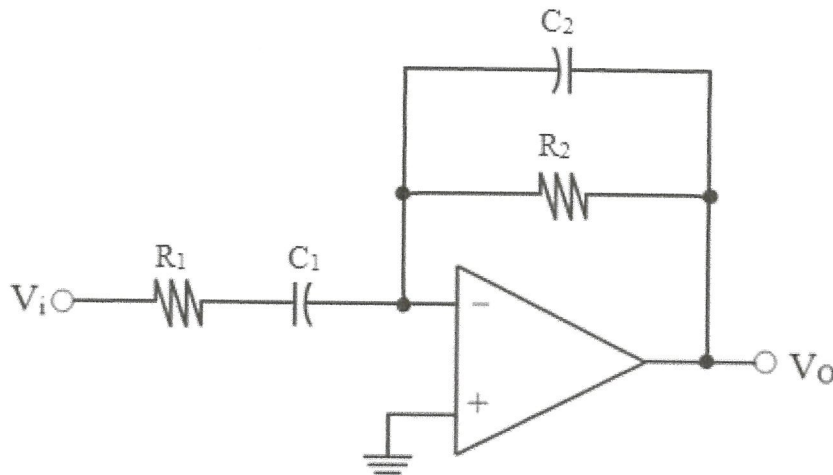


Figure Q2

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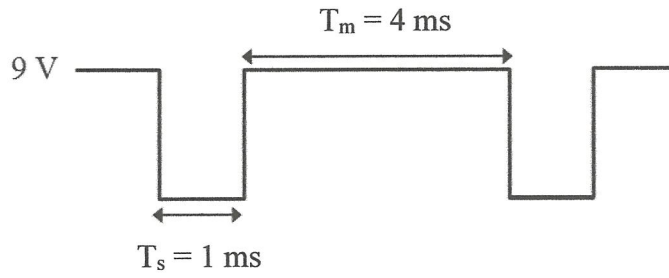


Figure Q4(c)

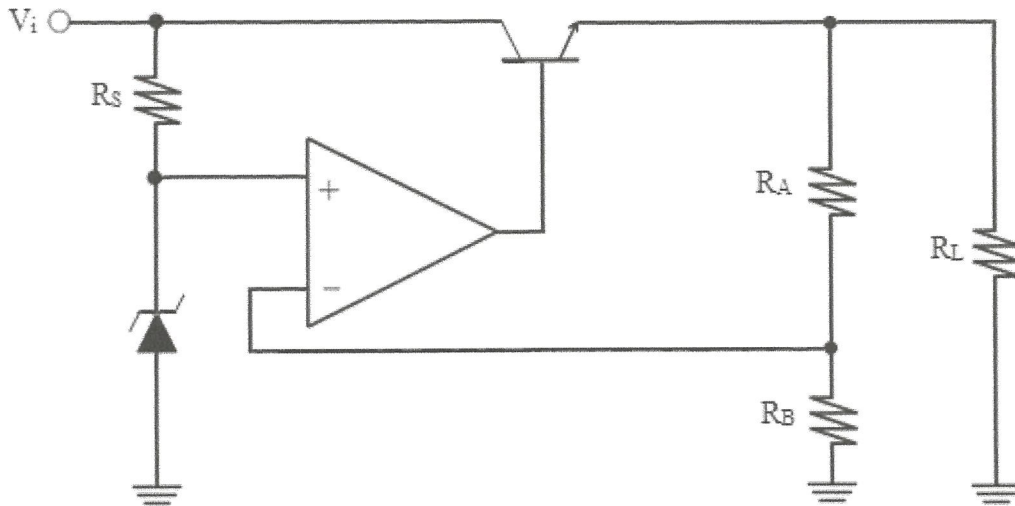


Figure Q5

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SEMESTER / SESSION : SEM II / 2017/2018 COURSE NAME : ELECTRONIC CIRCUITS ANALYSIS AND DESIGN PROGRAMME CODE : BEJ COURSE CODE : BEL 30403	
<b>Table 1 List of formula</b>	
Inverting Amplifier	$A_v = \frac{V_o}{V_i} = -\frac{R_f}{R_1}$
Non-Inverting Amplifier	$A_v = \frac{V_o}{V_i} = 1 + \frac{R_f}{R_1}$
Inverting Summing Amplifier	$V_o = -\left(\frac{R_f}{R_1}V_1 + \frac{R_f}{R_2}V_2 + \frac{R_f}{R_3}V_3\right)$
Non-Inverting Summing Amplifier	$V_o = \left(1 + \frac{R_f}{R_1}\right)\left(\frac{R_B}{R_A + R_B}V_A + \frac{R_A}{R_A + R_B}V_B\right)$
Subtracting Amplifier	$V_o = \left(1 + \frac{R_f}{R_1}\right)\left(\frac{R_3}{R_2 + R_3}V_2 - \frac{R_f}{R_1 + R_f}V_1\right)$
Instrumentation Amplifier	$A_T = A_1 A_2 = \frac{v_o}{v_{in}} = \left(1 + \frac{2R}{R_x}\right)\left(\frac{R_4}{R_3}\right)$
Integrator	$V_o(t) = -\frac{1}{RC} \int_{t_0}^t V_i(t) dt + V_o(t_0)$
Differentiator	$V_o(t) = -RC \frac{dV_i(t)}{dt}$
Schmitt Trigger	$V_{UTP \text{ or } LTP} = \frac{R_2}{R_1 + R_2}(\pm V_{out(max)}) + \frac{R_1}{R_1 + R_2}(V_{REF})$
Cut-off frequency for a filter	$f_c = \frac{1}{2\pi RC}$
1 <sup>st</sup> order Low Pass Filter	$A_v(s) = \frac{V_o}{V_i} = \left(1 + \frac{R_F}{R_1}\right)\left(\frac{1}{1 + sRC}\right)$
2 <sup>nd</sup> order Low pass filter	$A_v(s) = \frac{V_o}{V_i}(s) = \frac{A_{VO}}{(RCs)^2 + (3 - A_{VO})RCs + 1}$
1 <sup>st</sup> order High Pass Filter	$A_v(s) = \frac{V_o}{V_i} = \left(1 + \frac{R_F}{R_1}\right)\left(\frac{1}{1 + \frac{1}{sRC}}\right)$

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SEMESTER / SESSION : SEM II / 2017/2018	PROGRAMME CODE : BEJ
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**Table 1 List of formula (Cont..)**

2 <sup>nd</sup> order High Pass Filter	$A_v(s) = \frac{V_o}{V_i}(s) = \frac{A_{vo}}{\frac{1}{(sRC)^2} + \frac{3-A_{vo}}{sRC} + 1}$
Negative feedback – Gain	$A_f = \frac{V_o}{V_s} = \frac{A}{1 + \beta A}$
Positive feedback – Gain	$A_f = \frac{A}{1 - \beta A}$
Phase shift oscillator	$\beta = \frac{V_F}{V_o} = \frac{1}{\left(1 - \frac{5}{\omega^2 R^2 C^2}\right) + j\left(\frac{1}{\omega^3 R^3 C^3} - \frac{6}{\omega RC}\right)}$ <p>or</p> $\beta = \frac{V_F}{V_o} = \frac{1}{(1 - 5\omega^2 R^2 C^2) + j(6\omega RC - \omega^3 R^3 C^3)}$ $f_o = \frac{1}{2\pi RC\sqrt{6}} \quad \text{or} \quad f_o = \frac{\sqrt{6}}{2\pi RC}$
Wien bridge oscillator	$f_o = \frac{1}{2\pi\sqrt{R_1 R_2 C_1 C_2}}$
Colpitts Oscillator	$f_o = \frac{1}{2\pi\sqrt{LC_{eq}}} \quad C_{eq} = \frac{C_1 C_2}{C_1 + C_2}$
Hartley Oscillator	$f_o = \frac{1}{2\pi\sqrt{CL_{eq}}} \quad L_{eq} = L_1 + L_2$
UJT relaxation oscillator	$f_o = \frac{1}{R_T C_T \ln[1/(1-\eta)]}$

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<b>FINAL EXAMINATION</b>	
SEMESTER / SESSION : SEM II / 2017/2018 COURSE NAME : ELECTRONIC CIRCUITS ANALYSIS AND DESIGN PROGRAMME CODE : BEJ COURSE CODE : BEL 30403	
<b>Table 1 List of formula (Cont..)</b>	
Square wave Oscillator	$f = \frac{1}{T} = \frac{1}{2RC \ln\left(\frac{1+\beta}{1-\beta}\right)} \quad \beta = \frac{R_3}{R_3 + R_2}$
Triangular-wave Oscillator	$f = \frac{1}{4R_1C} \frac{R_2}{R_3}$
Capacitor voltage	$v_c(t) = v_c(0) + (v_c(\infty) - v_c(0)) \left(1 - e^{-t/\tau}\right)$ $= v_c(\infty) + (v_c(0) - v_c(\infty)) e^{-t/\tau}$
Astable Multivibrator	$T_m = t_1 = \tau_2 \ln 2 = 0.693(R_1 + R_2)C_1$ $T_s = t_2 = \tau_2 \ln 2 = 0.693R_2C_1$ $T = T_m + T_s$ $f = \frac{1.44}{(R_1 + 2R_2)C_1}$ $D = \frac{T_m}{T_m + T_s} \times 100\% = \frac{R_1 + R_2}{R_1 + 2R_2} \times 100\%$
Monostable Multivibrator	$T = 1.1 R_1 C_1$
Ripple Factor	$\% r = \frac{\text{ripple voltage (rms)}}{\text{dc voltage}} = \frac{V_{r(rms)}}{V_{dc}} \times 100$
Half-wave rectifier with a filter	$V_{r(rms)} = \frac{V_{r(p-p)}}{2\sqrt{3}} \approx \frac{V_{o(p)}}{2\sqrt{3} f C R_L}$ $V_{o(DC)} = V_{o(p)} - \frac{V_{r(p-p)}}{2} \quad V_{r(p-p)} \approx \frac{V_{o(p)}}{f C R_L} = \frac{I_{o(DC)}}{f C}$ $r = \frac{V_{r(rms)}}{V_{DC}} \approx \frac{1}{2\sqrt{3} f C R_L}$

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SEMESTER / SESSION : SEM II / 2017/2018	PROGRAMME CODE : BEJ
COURSE NAME : ELECTRONIC CIRCUITS ANALYSIS AND DESIGN	COURSE CODE : BEL 30403

**Table 1 List of formula (Cont..)**

Full-wave rectifier with a filter	$V_{r(rms)} = \frac{V_{r(p-p)}}{2\sqrt{3}} \approx \frac{V_{o(p)}}{4\sqrt{3}fCR_L} = \frac{I_{DC}}{4\sqrt{3}fC}$ $V_{o(DC)} = V_{o(p)} - \frac{V_{r(p-p)}}{2} \qquad V_{r(p-p)} = \frac{I_{o(DC)}}{2fC} \approx \frac{V_{o(p)}}{2fCR_L}$ $r = \frac{V_{r(rms)}}{V_{DC}} \approx \frac{1}{4\sqrt{3}fCR_L}$
Rectifier with Additional RC filter	$V'_{r(rms)} \approx \frac{X_C}{R} V_{r(rms)}$
Inductor Filter	$r = \frac{R_L}{3\sqrt{2}\omega L}$
Shunt regulator	$V_o \cong V_B \left( \frac{R_1 + R_2}{R_2} \right) \qquad V_B = V_Z + V_{BE}$ $V_o \cong \left( \frac{R_1 + R_2}{R_2} \right) (V_Z)$
Series regulator	$V_o = \frac{R_1 + R_2}{R_1} (V_Z + V_{BE}) \qquad V_o = V_Z \left( \frac{R_1 + R_2}{R_1} \right)$
Adjustable IC regulator	$V_o = V_{ref} \left( 1 + \frac{R_2}{R_1} \right) + I_{adj} R_2$

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