

**CONFIDENTIAL**



## **UNIVERSITI TUN HUSSEIN ONN MALAYSIA**

### **FINAL EXAMINATION SEMESTER I SESSION 2016/2017**

COURSE NAME	:	THERMODYNAMIC PROCESS
COURSE CODE	:	BNL 30203
PROGRAMME CODE	:	BNL
EXAMINATION DATE	:	DECEMBER 2016 / JANUARY 2017
DURATION	:	3 HOURS
INSTRUCTION	:	ANSWERS ALL QUESTIONS

**THIS QUESTION PAPER CONSISTS OF TEN (10) PAGES**

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**Q1** Consider a steam power plant that operates on a simple ideal Rankine cycle and has a net power output of 50 MW. Steam enters the turbine at 7 MPa and 500°C and is cooled in the condenser at a pressure of 20 kPa by running cooling water from a lake through the tubes of the condenser at a rate of 2500 kg/s. Thermodynamic data are given in **Table Q1**.

- (a) Sketch the thermodynamic cycle on a *T-s* diagram. Label 1 for the state before the pump. (4 marks)
- (b) Determine the thermal efficiency of the cycle. (10 marks)
- (c) Calculate the mass flow rate of the steam. (2 marks)
- (d) Determine the temperature rise of the cooling water where  $c_p = 4.18 \text{ kJ/kg.}^{\circ}\text{C}$ . (4 marks)

**Q2** (a) Explain how do the inefficiencies of the turbine and the compressor affect the back work ratio and the thermal efficiency of a gas-turbine engine. (2 marks)

- (b) Air enters the compressor of a regenerative gas-turbine engine at 300 K and 100 kPa, where it is compressed to 800 kPa and 580 K. The regenerator has an effectiveness of 72 percent, and air enters the turbine at 1200 K. The turbine efficiency is 86 percent. Thermodynamic data are given in **Table Q2**. (Assume variable specific heats for air).

- (i) Illustrate the thermodynamic cycle of the gas turbine with regeneration on a *T-s* diagram. (4 marks)
- (ii) Determine the amount of heat transfer in the regenerator. (10 marks)
- (iii) Calculate the thermal efficiency. (4 marks)

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- Q3** (a) When designing a refrigeration system, there are several refrigerants from which to choose, such as chlorofluorocarbons (CFCs), ammonia, hydrocarbons, carbon dioxide, air, and even water. The right choice of refrigerant depends on the situation at hand. Outline **FOUR (4)** desirable characteristics of a refrigerant that need to be considered in the selection of a refrigerant for a certain application.

(4 marks)

- (b) Consider a 300 kJ/min refrigeration system that operates on an ideal vapor-compression refrigeration cycle with refrigerant – 134a as the working fluid. The refrigerant enters the compressor as saturated vapor at 140 kPa and is compressed to 800 kPa. Thermodynamic data are given in **Table Q3**.

- (i) Show the cycle on a *T-s* diagram with respect to saturation lines. (4 marks)
- (ii) Determine the quality of the refrigerant at the end of the throttling process. (7 marks)
- (iii) Calculate the coefficient of performance. (3 marks)
- (iv) Calculate the power input to the compressor. (2 marks)

- Q4** (a) (i) List **FOUR (4)** processes that make up the Carnot cycle. (4 marks)

- (ii) A heat pump is used to maintain a house at a constant temperature of 34°C. The house is losing heat to the outside air through the walls and the windows at a rate of 60,000 kJ/h while the energy generated within the house from people, lights, and appliances amounts to 4000 kJ/h. For a COP of 2.5, calculate the required power input to the heat pump. (6 marks)

- (b) In a combustion chamber, ethane ( $C_2H_6$ ) is burned at a rate of 8 kg/h with air that enters the combustion chamber at a rate of 176 kg/h. Determine the percentage of excess air used during this process. (10 marks)

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- Q5** (a) In absorption refrigeration systems, a two-phase equilibrium mixture of liquid ammonia ( $\text{NH}_3$ ) and water ( $\text{H}_2\text{O}$ ) is frequently used. Consider a liquid-vapor mixture of ammonia and water in equilibrium at 30°C. The composition of the liquid phase is 70  $\text{NH}_3$  and 30 percent  $\text{H}_2\text{O}$  by mole numbers. Saturation pressure of  $\text{NH}_3$  and  $\text{H}_2\text{O}$  at 30°C is 1167.4 kPa and 4.247 kPa, respectively.
- (i) Determine the vapor pressure of  $\text{NH}_3$  and  $\text{H}_2\text{O}$  at 30°C. (4 marks)
- (ii) Calculate the total pressure of the mixture. (2 marks)
- (iii) Determine the composition of the vapor phase of this mixture. (4 marks)
- (b) Carbon dioxide ( $\text{CO}_2$ ) is heated to 2400 K at a constant pressure of 3 atm. Determine the percentage of  $\text{CO}_2$  that will dissociate into  $\text{CO}$  and  $\text{O}_2$  during this process. Given that the  $\ln K_p = -3.860$  at 2400 K, and the equilibrium constant relation can be expressed as

$$K_p = \frac{N_{CO}^{Vco} N_{O_2}^{VO_2}}{N_{CO_2}^{VC_02}} \left( \frac{P}{N_{total}} \right)^{(Vco+VO_2-VCO_2)}$$

(10 marks)

**-END OF QUESTIONS -****TERBUKA**

**CONFIDENTIAL****FINAL EXAMINATION**SEMESTER / SESSION : SEM I / 2016/2017  
COURSE NAME : THERMODYNAMIC PROCESSPROGRAMME CODE : BNL  
COURSE CODE : BNL 30203**TABLE Q1****Saturated water – pressure table**

Press., <i>P</i> kPa	Specific volume, m <sup>3</sup> /kg			Internal energy, kJ/kg			Enthalpy, kJ/kg			Entropy, kJ/kg · K		
	Sat. temp., <i>T<sub>sat</sub></i> °C	Sat. liquid, <i>v<sub>f</sub></i>	Sat. vapor, <i>v<sub>g</sub></i>	Sat. liquid, <i>u<sub>f</sub></i>	Evap., <i>u<sub>fg</sub></i>	Sat. vapor, <i>u<sub>g</sub></i>	Sat. liquid, <i>h<sub>f</sub></i>	Evap., <i>h<sub>fg</sub></i>	Sat. vapor, <i>h<sub>g</sub></i>	Sat. liquid, <i>s<sub>f</sub></i>	Sat. Evap., <i>s<sub>fg</sub></i>	Sat. vapor, <i>s<sub>g</sub></i>
1.0	6.97	0.001000	129.19	29.302	2355.2	2384.5	29.303	2484.4	2513.7	0.1059	8.8690	8.9749
1.5	13.02	0.001001	87.964	54.686	2338.1	2392.8	54.688	2470.1	2524.7	0.1956	8.6314	8.8270
2.0	17.50	0.001001	66.990	73.431	2325.5	2398.9	73.433	2459.5	2532.9	0.2606	8.4621	8.7227
2.5	21.08	0.001002	54.242	88.422	2315.4	2403.8	88.424	2451.0	2539.4	0.3118	8.3302	8.6421
3.0	24.08	0.001003	45.654	100.98	2306.9	2407.9	100.98	2443.9	2544.8	0.3543	8.2222	8.5765
4.0	28.96	0.001004	34.791	121.39	2293.1	2414.5	121.39	2432.3	2553.7	0.4224	8.0510	8.4734
5.0	32.87	0.001005	28.185	137.75	2282.1	2419.8	137.75	2423.0	2560.7	0.4762	7.9176	8.3938
7.5	40.29	0.001008	19.233	168.74	2261.1	2429.8	168.75	2405.3	2574.0	0.5763	7.6738	8.2501
10	45.81	0.001010	14.670	191.79	2245.4	2437.2	191.81	2392.1	2583.9	0.6492	7.4996	8.1488
15	53.97	0.001014	10.020	225.93	2222.1	2448.0	225.94	2372.3	2598.3	0.7549	7.2522	8.0071
20	60.06	0.001017	7.6481	251.40	2204.6	2456.0	251.42	2357.5	2608.9	0.8320	7.0752	7.9073
25	64.96	0.001020	6.2034	271.93	2190.4	2462.4	271.96	2345.5	2617.5	0.8932	6.9370	7.8302
30	69.09	0.001022	5.2287	289.24	2178.5	2467.7	289.27	2335.3	2624.6	0.9441	6.8234	7.7675
40	75.86	0.001026	3.9933	317.58	2158.8	2476.3	317.62	2318.4	2636.1	1.0261	6.6430	7.6691
50	81.32	0.001030	3.2403	340.49	2142.7	2483.2	340.54	2304.7	2645.2	1.0912	6.5019	7.5931

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## FINAL EXAMINATION

SEMESTER / SESSION : SEM I / 2016/2017  
 COURSE NAME : THERMODYNAMIC PROCESS

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 COURSE CODE : BNL 30203

TABLE Q1

Superheated water

T °C	v m³/kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m³/kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m³/kg	u kJ/kg	h kJ/kg	s kJ/kg · K
$P = 6.0 \text{ MPa (275.59°C)}$					$P = 7.0 \text{ MPa (285.83°C)}$					$P = 8.0 \text{ MPa (295.01°C)}$		
Sat.	0.03245	2589.9	2784.6	5.8902	0.027378	2581.0	2772.6	5.8148	0.023525	2570.5	2758.7	5.7450
300	0.03619	2668.4	2885.6	6.0703	0.029492	2633.5	2839.9	5.9337	0.024279	2592.3	2786.5	5.7937
350	0.04225	2790.4	3043.9	6.3357	0.035262	2770.1	3016.9	6.2305	0.029975	2748.3	2988.1	6.1321
400	0.04742	2893.7	3178.3	6.5432	0.039958	2879.5	3159.2	6.4502	0.034344	2864.6	3139.4	6.3658
450	0.05217	2989.9	3302.9	6.7219	0.044187	2979.0	3288.3	6.6353	0.038194	2967.8	3273.3	6.5579
500	0.05667	3083.1	3423.1	6.8826	0.048157	3074.3	3411.4	6.8000	0.041767	3065.4	3399.5	6.7266
550	0.06102	3175.2	3541.3	7.0308	0.051966	3167.9	3531.6	6.9507	0.045172	3160.5	3521.8	6.8800
600	0.06527	3267.2	3658.8	7.1693	0.055665	3261.0	3650.6	7.0910	0.048463	3254.7	3642.4	7.0221
700	0.07355	3453.0	3894.3	7.4247	0.062850	3448.3	3888.3	7.3487	0.054829	3443.6	3882.2	7.2822
800	0.08165	3643.2	4133.1	7.6582	0.069856	3639.5	4128.5	7.5836	0.061011	3635.7	4123.8	7.5185
900	0.08964	3838.8	4376.6	7.8751	0.076750	3835.7	4373.0	7.8014	0.067082	3832.7	4369.3	7.7372
1000	0.09756	4040.1	4625.4	8.0786	0.083571	4037.5	4622.5	8.0055	0.073079	4035.0	4619.6	7.9419
1100	0.10543	4247.1	4879.7	8.2709	0.090341	4245.0	4877.4	8.1982	0.079025	4242.8	4875.0	8.1350
1200	0.11326	4459.8	5139.4	8.4534	0.097075	4457.9	5137.4	8.3810	0.084934	4456.1	5135.5	8.3181
1300	0.12107	4677.7	5404.1	8.6273	0.103781	4676.1	5402.6	8.5551	0.090817	4674.5	5401.0	8.4925
$P = 2.50 \text{ MPa (223.95°C)}$					$P = 3.00 \text{ MPa (233.85°C)}$					$P = 3.50 \text{ MPa (242.56°C)}$		
Sat.	0.07995	2602.1	2801.9	6.2558	0.066667	2603.2	2803.2	6.1856	0.05706	2603.0	2802.7	6.1244
225	0.08026	2604.8	2805.5	6.2629	0.07063	2644.7	2856.5	6.2893	0.05876	2624.0	2829.7	6.1764
250	0.08705	2663.3	2880.9	6.4107	0.08118	2750.8	2994.3	6.5412	0.06845	2738.8	2978.4	6.4484
300	0.09894	2762.2	3009.6	6.6459	0.09056	2844.4	3116.1	6.7450	0.07680	2836.0	3104.9	6.6601
350	0.10979	2852.5	3127.0	6.8424	0.10789	2933.6	3231.7	6.9235	0.08456	2927.2	3223.2	6.8428
400	0.12012	2939.8	3240.1	7.0170	0.11620	3108.6	3457.2	7.2359	0.09198	3016.1	3338.1	7.0074
450	0.13015	3026.2	3351.6	7.1768	0.12420	3192.4	3517.2	7.4059	0.09919	3104.5	3451.7	7.1593
500	0.13999	3112.8	3462.8	7.3254	0.13245	3285.5	3682.8	7.5103	0.11325	3282.5	3678.9	7.4357
600	0.15931	3288.5	3686.8	7.5979	0.14841	3467.0	3912.2	7.7590	0.12702	3464.7	3909.3	7.6855
700	0.17835	3469.3	3915.2	7.8455	0.16420	3654.3	4146.9	7.9885	0.14061	3652.5	4144.6	7.9156
800	0.19722	3656.2	4149.2	8.0744	0.17988	3847.9	4387.5	8.2028	0.15410	3846.4	4385.7	8.1304
900	0.21597	3849.4	4389.3	8.2882	0.19549	4047.7	4634.2	8.4045	0.16751	4046.4	4632.7	8.3324
1000	0.23466	4049.0	4635.6	8.4897	0.21105	4253.6	4886.7	8.5955	0.18087	4252.5	4885.6	8.5236
1100	0.25330	4254.7	4887.9	8.6804	0.22658	4465.3	5145.1	8.7771	0.19420	4464.4	5144.1	8.7053
1200	0.27190	4466.3	5146.0	8.8618	0.24207	4682.6	5408.8	8.9502	0.20750	4681.8	5408.0	8.8786

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## FINAL EXAMINATION

SEMESTER / SESSION : SEM I / 2016/2017  
 COURSE NAME : THERMODYNAMIC PROCESS

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TABLE Q2

Ideal-gas properties of air

T K	<i>h</i> kJ/kg	<i>P<sub>r</sub></i>	<i>u</i> kJ/kg	<i>v<sub>r</sub></i>	<i>s<sup>o</sup></i> kJ/kg · K	T K	<i>h</i> kJ/kg	<i>P<sub>r</sub></i>	<i>u</i> kJ/kg	<i>v<sub>r</sub></i>	<i>s<sup>o</sup></i> kJ/kg · K
200	199.97	0.3363	142.56	1707.0	1.29559	580	586.04	14.38	419.55	115.7	2.37348
210	209.97	0.3987	149.69	1512.0	1.34444	590	596.52	15.31	427.15	110.6	2.39140
220	219.97	0.4690	156.82	1346.0	1.39105	600	607.02	16.28	434.78	105.8	2.40902
230	230.02	0.5477	164.00	1205.0	1.43557	610	617.53	17.30	442.42	101.2	2.42644
240	240.02	0.6355	171.13	1084.0	1.47824	620	628.07	18.36	450.09	96.92	2.44356
250	250.05	0.7329	178.28	979.0	1.51917	630	638.63	19.84	457.78	92.84	2.46048
260	260.09	0.8405	185.45	887.8	1.55848	640	649.22	20.64	465.50	88.99	2.47716
270	270.11	0.9590	192.60	808.0	1.59634	650	659.84	21.86	473.25	85.34	2.49364
280	280.13	1.0889	199.75	738.0	1.63279	660	670.47	23.13	481.01	81.89	2.50985
285	285.14	1.1584	203.33	706.1	1.65055	670	681.14	24.46	488.81	78.61	2.52589
290	290.16	1.2311	206.91	676.1	1.66802	680	691.82	25.85	496.62	75.50	2.54175
295	295.17	1.3068	210.49	647.9	1.68515	690	702.52	27.29	504.45	72.56	2.55731
298	298.18	1.3543	212.64	631.9	1.69528	700	713.27	28.80	512.33	69.76	2.57277
300	300.19	1.3860	214.07	621.2	1.70203	710	724.04	30.38	520.23	67.07	2.58810
305	305.22	1.4686	217.67	596.0	1.71865	720	734.82	32.02	528.14	64.53	2.60319
310	310.24	1.5546	221.25	572.3	1.73498	730	745.62	33.72	536.07	62.13	2.61803
315	315.27	1.6442	224.85	549.8	1.75106	740	756.44	35.50	544.02	59.82	2.63280
320	320.29	1.7375	228.42	528.6	1.76690	750	767.29	37.35	551.99	57.63	2.64737
325	325.31	1.8345	232.02	508.4	1.78249	760	778.18	39.27	560.01	55.54	2.66176
330	330.34	1.9352	235.61	489.4	1.79783	780	800.03	43.35	576.12	51.64	2.69013
340	340.42	2.149	242.82	454.1	1.82790	800	821.95	47.75	592.30	48.08	2.71787
350	350.49	2.379	250.02	422.2	1.85708	820	843.98	52.59	608.59	44.84	2.74504
360	360.58	2.626	257.24	393.4	1.88543	840	866.08	57.60	624.95	41.85	2.77170
370	370.67	2.892	264.46	367.2	1.91313	860	888.27	63.09	641.40	39.12	2.79783
380	380.77	3.176	271.69	343.4	1.94001	880	910.56	68.98	657.95	36.61	2.82344
390	390.88	3.481	278.93	321.5	1.96633	900	932.93	75.29	674.58	34.31	2.84856
400	400.98	3.806	286.16	301.6	1.99194	920	955.38	82.05	691.28	32.18	2.87324
410	411.12	4.153	293.43	283.3	2.01699	940	977.92	89.28	708.08	30.22	2.89748
420	421.26	4.522	300.69	266.6	2.04142	960	1000.55	97.00	725.02	28.40	2.92128
430	431.43	4.915	307.99	251.1	2.06533	980	1023.25	105.2	741.98	26.73	2.94468
440	441.61	5.332	315.30	236.8	2.08870	1000	1046.04	114.0	758.94	25.17	2.96770
450	451.80	5.775	322.62	223.6	2.11161	1020	1068.89	123.4	776.10	23.72	2.99034
460	462.02	6.245	329.97	211.4	2.13407	1040	1091.85	133.3	793.36	23.29	3.01260
470	472.24	6.742	337.32	200.1	2.15604	1060	1114.86	143.9	810.62	21.14	3.03449
480	482.49	7.268	344.70	189.5	2.17760	1080	1137.89	155.2	827.88	19.98	3.05608
490	492.74	7.824	352.08	179.7	2.19876	1100	1161.07	167.1	845.33	18.896	3.07732
500	503.02	8.411	359.49	170.6	2.21952	1120	1184.28	179.7	862.79	17.886	3.09825
510	513.32	9.031	366.92	162.1	2.23993	1140	1207.57	193.1	880.35	16.946	3.11883
520	523.63	9.684	374.36	154.1	2.25997	1160	1230.92	207.2	897.91	16.064	3.13916
530	533.98	10.37	381.84	146.7	2.27967	1180	1254.34	222.2	915.57	15.241	3.15916
540	544.35	11.10	389.34	139.7	2.29906	1200	1277.79	238.0	933.33	14.470	3.17888
550	555.74	11.86	396.86	133.1	2.31809	1220	1301.31	254.7	951.09	13.747	3.19834
560	565.17	12.66	404.42	127.0	2.33685	1240	1324.93	272.3	968.95	13.069	3.21751
570	575.59	13.50	411.97	121.2	2.35531						

## FINAL EXAMINATION

SEMESTER / SESSION : SEM I / 2016/2017  
 COURSE NAME : THERMODYNAMIC PROCESS

PROGRAMME CODE : BNL  
 COURSE CODE : BNL 30203

TABLE Q3

Saturated refrigerant-134 a – Pressure table

Press., P kPa	Sat. $T_{sat}$ , °C	Specific volume, m³/kg		Internal energy, kJ/kg			Enthalpy, kJ/kg			Entropy, kJ/kg · K		
		Sat. liquid, $v_f$	Sat. vapor, $v_g$	Sat. liquid, $u_f$	Evap., $u_{fg}$	Sat. vapor, $u_g$	Sat. liquid, $h_f$	Evap., $h_{fg}$	Sat. vapor, $h_g$	Sat. liquid, $s_f$	Evap., $s_{fg}$	Sat. vapor, $s_g$
60	-36.95	0.0007098	0.31121	3.798	205.32	209.12	3.841	223.95	227.79	0.01634	0.94807	0.96441
70	-33.87	0.0007144	0.26929	7.680	203.20	210.88	7.730	222.00	229.73	0.03267	0.92775	0.96042
80	-31.13	0.0007185	0.23753	11.15	201.30	212.46	11.21	220.25	231.46	0.04711	0.90999	0.95710
90	-28.65	0.0007223	0.21263	14.31	199.57	213.88	14.37	218.65	233.02	0.06008	0.89419	0.95427
100	-26.37	0.0007259	0.19254	17.21	197.98	215.19	17.28	217.16	234.44	0.07188	0.87995	0.95183
120	-22.32	0.0007324	0.16212	22.40	195.11	217.51	22.49	214.48	236.97	0.09275	0.85503	0.94779
140	-18.77	0.0007383	0.14014	26.98	192.57	219.54	27.08	212.08	239.16	0.11087	0.83368	0.94456
160	-15.60	0.0007437	0.12348	31.09	190.27	221.35	31.21	209.90	241.11	0.12693	0.81496	0.94190
180	-12.73	0.0007487	0.11041	34.83	188.16	222.99	34.97	207.90	242.86	0.14139	0.79826	0.93965
200	-10.09	0.0007533	0.099867	38.28	186.21	224.48	38.43	206.03	244.46	0.15457	0.78316	0.93773
240	-5.38	0.0007620	0.083897	44.48	182.67	227.14	44.66	202.62	247.28	0.17794	0.75664	0.93458
280	-1.25	0.0007699	0.072352	49.97	179.50	229.46	50.18	199.54	249.72	0.19829	0.73381	0.93210
320	2.46	0.0007772	0.063604	54.92	176.61	231.52	55.16	196.71	251.88	0.21637	0.71369	0.93006
360	5.82	0.0007841	0.056738	59.44	173.94	233.38	59.72	194.08	253.81	0.23270	0.69566	0.92836
400	8.91	0.0007907	0.051201	63.62	171.45	235.07	63.94	191.62	255.55	0.24761	0.67929	0.92691
450	12.46	0.0007985	0.045619	68.45	168.54	237.00	68.81	188.71	257.53	0.26465	0.66069	0.92535
500	15.71	0.0008059	0.041118	72.93	165.82	238.75	73.33	185.98	259.30	0.28023	0.64377	0.92400
550	18.73	0.0008130	0.037408	77.10	163.25	240.35	77.54	183.38	260.92	0.29461	0.62821	0.92282
600	21.55	0.0008199	0.034295	81.02	160.81	241.83	81.51	180.90	262.40	0.30799	0.61378	0.92177
650	24.20	0.0008266	0.031646	84.72	158.48	243.20	85.26	178.51	263.77	0.32051	0.60030	0.92081
700	26.69	0.0008331	0.029361	88.24	156.24	244.48	88.82	176.21	265.03	0.33230	0.58763	0.91994
750	29.06	0.0008395	0.027371	91.59	154.08	245.67	92.22	173.98	266.20	0.34345	0.57567	0.91912
800	31.31	0.0008458	0.025621	94.79	152.00	246.79	95.47	171.82	267.29	0.35404	0.56431	0.91835
850	33.45	0.0008520	0.024069	97.87	149.98	247.85	98.60	169.71	268.31	0.36413	0.55349	0.91762
900	35.51	0.0008580	0.022683	100.83	148.01	248.85	101.61	167.66	269.26	0.37377	0.54315	0.91692
950	37.48	0.0008641	0.021438	103.69	146.10	249.79	104.51	165.64	270.15	0.38301	0.53323	0.91624
1000	39.37	0.0008700	0.020313	106.45	144.23	250.68	107.32	163.67	270.99	0.39189	0.52368	0.91558
1200	46.29	0.0008934	0.016715	116.70	137.11	253.81	117.77	156.10	273.87	0.42441	0.48863	0.91303
1400	52.40	0.0009166	0.014107	125.94	130.43	256.37	127.22	148.90	276.12	0.45315	0.45734	0.91050
1600	57.88	0.0009400	0.012123	134.43	124.04	258.47	135.93	141.93	277.86	0.47911	0.42873	0.90784
1800	62.87	0.0009639	0.010559	142.33	117.83	260.17	144.07	135.11	279.17	0.50294	0.40204	0.90498
2000	67.45	0.0009886	0.009288	149.78	111.73	261.51	151.76	128.33	280.09	0.52509	0.37675	0.90184
2500	77.54	0.0010566	0.006936	166.99	96.47	263.45	169.63	111.16	280.79	0.57531	0.31695	0.89226
3000	86.16	0.0011406	0.005275	183.04	80.22	263.26	186.46	92.63	279.09	0.62118	0.25776	0.87894

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## FINAL EXAMINATION

SEMESTER / SESSION : SEM I / 2016/2017  
 COURSE NAME : THERMODYNAMIC PROCESS

PROGRAMME CODE : BNL  
 COURSE CODE : BNL 30203

TABLE Q3  
 Superheated refrigerant-134a

T °C	v m³/kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m³/kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m³/kg	u kJ/kg	h kJ/kg	s kJ/kg · K
$P = 0.06 \text{ MPa } (T_{\text{sat}} = -36.95^\circ\text{C})$					$P = 0.10 \text{ MPa } (T_{\text{sat}} = -26.37^\circ\text{C})$					$P = 0.14 \text{ MPa } (T_{\text{sat}} = -18.77^\circ\text{C})$		
Sat.	0.31121	209.12	227.79	0.9644	0.19254	215.19	234.44	0.9518	0.14014	219.54	239.16	0.9446
-20	0.33608	220.60	240.76	1.0174	0.19841	219.66	239.50	0.9721	0.14605	225.91	246.36	0.9724
-10	0.35048	227.55	248.58	1.0477	0.20743	226.75	247.49	1.0030	0.15263	233.23	254.60	1.0031
0	0.36476	234.66	256.54	1.0774	0.21630	233.95	255.58	1.0332	0.15908	240.66	262.93	1.0331
10	0.37893	241.92	264.66	1.1066	0.22506	241.30	263.81	1.0628	0.16544	248.22	271.38	1.0624
20	0.39302	249.35	272.94	1.1353	0.23373	248.79	272.17	1.0918	0.17172	255.93	279.97	1.0912
30	0.40705	256.95	281.37	1.1636	0.24233	256.44	280.68	1.1203	0.17794	263.79	288.70	1.1195
40	0.42102	264.71	289.97	1.1915	0.25088	264.25	289.34	1.1484	0.18412	271.79	297.57	1.1474
50	0.43495	272.64	298.74	1.2191	0.25937	272.22	298.16	1.1762	0.19025	279.96	306.59	1.1749
60	0.44883	280.73	307.66	1.2463	0.26783	280.35	307.13	1.2035	0.19635	288.28	315.77	1.2020
70	0.46269	288.99	316.75	1.2732	0.27626	288.64	316.26	1.2305	0.20242	296.75	325.09	1.2288
80	0.47651	297.41	326.00	1.2997	0.28465	297.08	325.55	1.2572	0.20847	305.38	334.57	1.2553
90	0.49032	306.00	335.42	1.3260	0.29303	305.69	334.99	1.2836	0.21449	314.17	344.20	1.2814
100	0.50410	314.74	344.99	1.3520	0.30138	314.46	344.60	1.3096				
$P = 0.18 \text{ MPa } (T_{\text{sat}} = -12.73^\circ\text{C})$					$P = 0.20 \text{ MPa } (T_{\text{sat}} = -10.09^\circ\text{C})$					$P = 0.24 \text{ MPa } (T_{\text{sat}} = -5.38^\circ\text{C})$		
Sat.	0.11041	222.99	242.86	0.9397	0.09987	224.48	244.46	0.9377	0.08390	227.14	247.28	0.9346
-10	0.11189	225.02	245.16	0.9484	0.09991	224.55	244.54	0.9380	0.08617	231.29	251.97	0.9519
0	0.11722	232.48	253.58	0.9798	0.10481	232.09	253.05	0.9698	0.09026	238.98	260.65	0.9831
10	0.12240	240.00	262.04	1.0102	0.10955	239.67	261.58	1.0004	0.09423	246.74	269.36	1.0134
20	0.12748	247.64	270.59	1.0399	0.11418	247.35	270.18	1.0303	0.10193	262.59	287.06	1.0718
30	0.13248	255.41	279.25	1.0690	0.11874	255.14	278.89	1.0595	0.10570	270.71	296.08	1.1001
40	0.13741	263.31	288.05	1.0975	0.12322	263.08	287.72	1.0882	0.11310	287.36	314.51	1.1554
50	0.14230	271.36	296.98	1.1256	0.12766	271.15	296.68	1.1163	0.11675	295.91	323.93	1.1825
60	0.14715	279.56	306.05	1.1532	0.13206	279.37	305.78	1.1441	0.12038	304.60	333.49	1.2092
70	0.15196	287.91	315.27	1.1805	0.13641	287.73	315.01	1.1714	0.12398	313.44	343.20	1.2356
80	0.15673	296.42	324.63	1.2074	0.14074	296.25	324.40	1.1983				
90	0.16149	305.07	334.14	1.2339	0.14504	304.92	333.93	1.2249				
100	0.16622	313.88	343.80	1.2602	0.14933	313.74	343.60	1.2512				
$P = 0.28 \text{ MPa } (T_{\text{sat}} = -1.25^\circ\text{C})$					$P = 0.32 \text{ MPa } (T_{\text{sat}} = 2.46^\circ\text{C})$					$P = 0.40 \text{ MPa } (T_{\text{sat}} = 8.91^\circ\text{C})$		
Sat.	0.07235	229.46	249.72	0.9321	0.06360	231.52	251.88	0.9301	0.051201	235.07	255.55	0.9269
0	0.07282	230.44	250.83	0.9362	0.06609	237.54	258.69	0.9544	0.051506	235.97	256.58	0.9305
10	0.07646	238.27	259.68	0.9680	0.06925	245.50	267.66	0.9856	0.054213	244.18	265.86	0.9628
20	0.07997	246.13	268.52	0.9987	0.07231	253.50	276.65	1.0157	0.056796	252.36	275.07	0.9937
30	0.08338	254.06	277.41	1.0285	0.07530	261.60	285.70	1.0451	0.059292	260.58	284.30	1.0236
40	0.08672	262.10	286.38	1.0576	0.07823	269.82	294.85	1.0739	0.061724	268.90	293.59	1.0528
50	0.09000	270.27	295.47	1.0862	0.08111	278.15	304.11	1.1021	0.064104	277.32	302.96	1.0814
60	0.09324	278.56	304.67	1.1142	0.08395	286.62	313.48	1.1298	0.066443	285.86	312.44	1.1094
70	0.09644	286.99	314.00	1.1418	0.08675	295.22	322.98	1.1571	0.068747	294.53	322.02	1.1369
80	0.09961	295.57	323.46	1.1690	0.09053	303.97	332.62	1.1840	0.070123	303.32	331.73	1.1640
90	0.10275	304.29	333.06	1.1958	0.09229	312.86	342.39	1.2105	0.073274	312.26	341.57	1.1907
100	0.10587	313.15	342.80	1.2222	0.09503	321.89	352.30	1.2367	0.075504	321.33	351.53	1.2171
110	0.10897	322.16	352.68	1.2483	0.09775	331.07	362.35	1.2626	0.077717	330.55	361.63	1.2431
120	0.11205	331.32	362.70	1.2742	0.10045	340.39	372.54	1.2882	0.079913	339.90	371.87	1.2688
130	0.11512	340.63	372.87	1.2997	0.10314	349.86	382.87	1.3135	0.082096	349.41	382.24	1.2942

## FINAL EXAMINATION

SEMESTER / SESSION : SEM I / 2016/2017  
 COURSE NAME : THERMODYNAMIC PROCESS

PROGRAMME CODE : BNL  
 COURSE CODE : BNL 30203

TABLE Q3

Superheated refrigerant-134a (*continued...*)

T °C	v m³/kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m³/kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m³/kg	u kJ/kg	h kJ/kg	s kJ/kg · K
$P = 0.50 \text{ MPa } (T_{sat} = 15.71^\circ\text{C})$					$P = 0.60 \text{ MPa } (T_{sat} = 21.55^\circ\text{C})$					$P = 0.70 \text{ MPa } (T_{sat} = 26.69^\circ\text{C})$		
Sat.	0.041118	238.75	259.30	0.9240	0.034295	241.83	262.40	0.9218	0.029361	244.48	265.03	0.9199
20	0.042115	242.40	263.46	0.9383								
30	0.044338	250.84	273.01	0.9703	0.035984	249.22	270.81	0.9499	0.029966	247.48	268.45	0.9313
40	0.046456	259.26	282.48	1.0011	0.037865	257.86	280.58	0.9816	0.031696	256.39	278.57	0.9641
50	0.048499	267.72	291.96	1.0309	0.039659	266.48	290.28	1.0121	0.033322	265.20	288.53	0.9954
60	0.050485	276.25	301.50	1.0599	0.041389	275.15	299.98	1.0417	0.034875	274.01	298.42	1.0256
70	0.052427	284.89	311.10	1.0883	0.043069	283.89	309.73	1.0705	0.036373	282.87	308.33	1.0549
80	0.054331	293.64	320.80	1.1162	0.044710	292.73	319.55	1.0987	0.037829	291.80	318.28	1.0835
90	0.056205	302.51	330.61	1.1436	0.046318	301.67	329.46	1.1264	0.039250	300.82	328.29	1.1114
100	0.058053	311.50	340.53	1.1705	0.047900	310.73	339.47	1.1536	0.040642	309.95	338.40	1.1389
110	0.059880	320.63	350.57	1.1971	0.049458	319.91	349.59	1.1803	0.042010	319.19	348.60	1.1658
120	0.061687	329.89	360.73	1.2233	0.050997	329.23	359.82	1.2067	0.043358	328.55	358.90	1.1924
130	0.063479	339.29	371.03	1.2491	0.052519	338.67	370.18	1.2327	0.044688	338.04	369.32	1.2186
140	0.065256	348.83	381.46	1.2747	0.054027	348.25	380.66	1.2584	0.046004	347.66	379.86	1.2444
150	0.067021	358.51	392.02	1.2999	0.055522	357.96	391.27	1.2838	0.047306	357.41	390.52	1.2699
160	0.068775	368.33	402.72	1.3249	0.057006	367.81	402.01	1.3088	0.048597	367.29	401.31	1.2951
$P = 0.80 \text{ MPa } (T_{sat} = 31.31^\circ\text{C})$					$P = 0.90 \text{ MPa } (T_{sat} = 35.51^\circ\text{C})$					$P = 1.00 \text{ MPa } (T_{sat} = 39.37^\circ\text{C})$		
Sat.	0.025621	246.79	267.29	0.9183	0.022683	248.85	269.26	0.9169	0.020313	250.68	270.99	0.9156
40	0.027035	254.82	276.45	0.9480	0.023375	253.13	274.17	0.9327	0.020406	251.30	271.71	0.9179
50	0.028547	263.86	286.69	0.9802	0.024809	262.44	284.77	0.9660	0.021796	260.94	282.74	0.9525
60	0.029973	272.83	296.81	1.0110	0.026146	271.60	295.13	0.9976	0.023068	270.32	293.38	0.9850
70	0.031340	281.81	306.88	1.0408	0.027413	280.72	305.39	1.0280	0.024261	279.59	303.85	1.0160
80	0.032659	290.84	316.97	1.0698	0.028630	289.86	315.63	1.0574	0.025398	288.86	314.25	1.0458
90	0.033941	299.95	327.10	1.0981	0.029806	299.06	325.89	1.0860	0.026492	298.15	324.64	1.0748
100	0.035193	309.15	337.30	1.1258	0.030951	308.34	336.19	1.1140	0.027552	307.51	335.06	1.1031
110	0.036420	318.45	347.59	1.1530	0.032068	317.70	346.56	1.1414	0.028584	316.94	345.53	1.1308
120	0.037625	327.87	357.97	1.1798	0.033164	327.18	357.02	1.1684	0.029592	326.47	356.06	1.1580
130	0.038813	337.40	368.45	1.2061	0.034241	336.76	367.58	1.1949	0.030581	336.11	366.69	1.1846
140	0.039985	347.06	379.05	1.2321	0.035302	346.46	378.23	1.2210	0.031554	345.85	377.40	1.2109
150	0.041143	356.85	389.76	1.2577	0.036349	356.28	389.00	1.2467	0.032512	355.71	388.22	1.2368
160	0.042290	366.76	400.59	1.2830	0.037384	366.23	399.88	1.2721	0.033457	365.70	399.15	1.2623
170	0.043427	376.81	411.55	1.3080	0.038408	376.31	410.88	1.2972	0.034392	375.81	410.20	1.2875
180	0.044554	386.99	422.64	1.3327	0.039423	386.52	422.00	1.3221	0.035317	386.04	421.36	1.3124
$P = 1.20 \text{ MPa } (T_{sat} = 46.29^\circ\text{C})$					$P = 1.40 \text{ MPa } (T_{sat} = 52.40^\circ\text{C})$					$P = 1.60 \text{ MPa } (T_{sat} = 57.88^\circ\text{C})$		
Sat.	0.016715	253.81	273.87	0.9130	0.014107	256.37	276.12	0.9105	0.012123	258.47	277.86	0.9078
50	0.017201	257.63	278.27	0.9267								
60	0.018404	267.56	289.64	0.9614	0.015005	264.46	285.47	0.9389	0.012372	260.89	280.69	0.9163
70	0.019502	277.21	300.61	0.9938	0.016060	274.62	297.10	0.9733	0.013430	271.76	293.25	0.9535
80	0.020529	286.75	311.39	1.0248	0.017023	284.51	308.34	1.0056	0.014362	282.09	305.07	0.9875
90	0.021506	296.26	322.07	1.0546	0.017923	294.28	319.37	1.0364	0.015215	292.17	316.52	1.0194
100	0.022442	305.80	332.73	1.0836	0.018778	304.01	330.30	1.0661	0.016014	302.14	327.76	1.0500
110	0.023348	315.38	343.40	1.1118	0.019597	313.76	341.19	1.0949	0.016773	312.07	338.91	1.0795
120	0.024228	325.03	354.11	1.1394	0.020388	323.55	352.09	1.1230	0.017500	322.02	350.02	1.1081
130	0.025086	334.77	364.88	1.1664	0.021155	333.41	363.02	1.1504	0.018201	332.00	361.12	1.1360
140	0.025927	344.61	375.72	1.1930	0.021904	343.34	374.01	1.1773	0.018882	342.05	372.26	1.1632
150	0.026753	354.56	386.66	1.2192	0.022636	353.37	385.07	1.2038	0.019545	352.17	383.44	1.1900
160	0.027566	364.61	397.69	1.2449	0.023355	363.51	396.20	1.2298	0.020194	362.38	394.69	1.2163
170	0.028367	374.78	408.82	1.2703	0.024061	373.75	407.43	1.2554	0.020830	372.69	406.02	1.2421
180	0.029158	385.08	420.07	1.2954	0.024757	384.10	418.76	1.2807	0.021456	383.11	417.44	1.2676

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